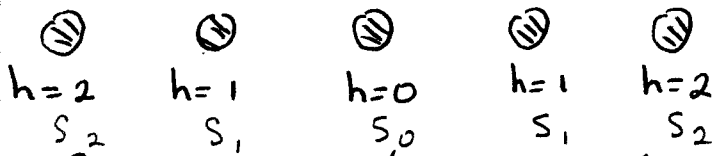


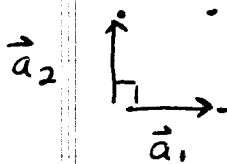
Spots on detector ("reflexes")



Spacings proportional to  $\frac{1}{a} \equiv a^*$  and  $\lambda$

small  $a \rightarrow$  large  $a^*$        $\beta = h \lambda a^*$   
 large  $a \rightarrow$  small  $a^*$

Now consider a 2D surface lattice:



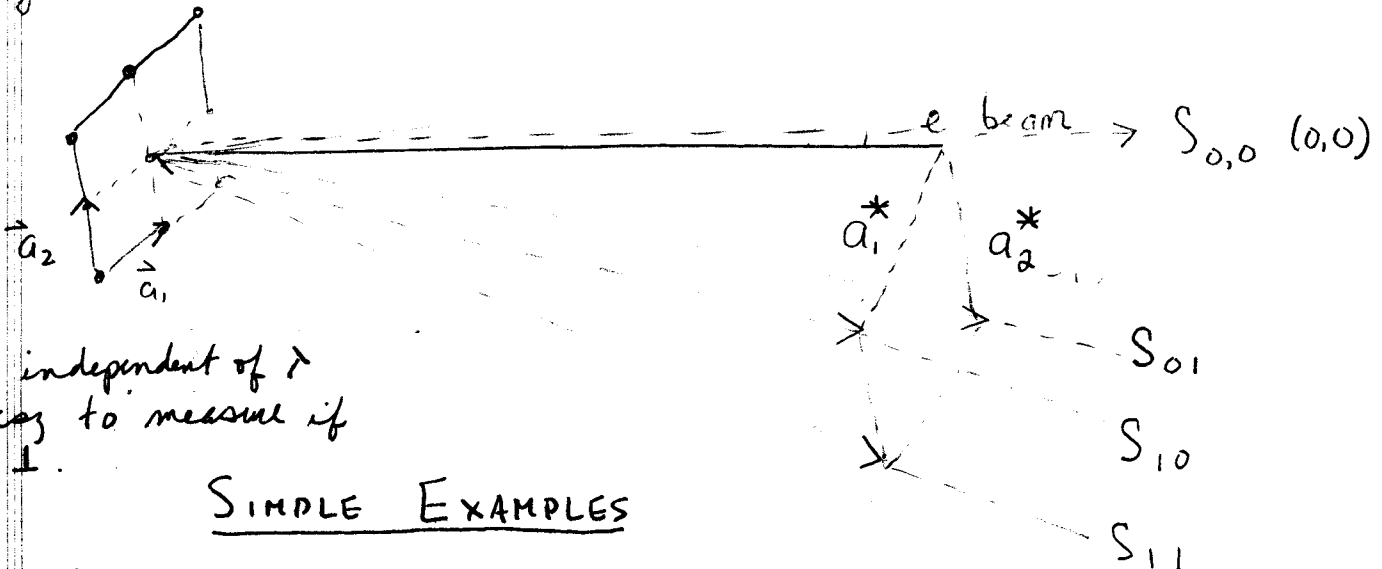
For each dimension of periodicity, there is a diffraction equation:

$$a_1 \cos \alpha_1 = a_1 \sin \beta_1 = h_1 \lambda$$

$$a_2 \cos \alpha_2 = a_2 \sin \beta_2 = h_2 \lambda$$

$$\beta_1 = \frac{h_1 \lambda}{a_1} \quad \beta_2 = \frac{h_2 \lambda}{a_2} \quad \text{or} \quad \beta_1 = h_1 \lambda a_1^* \quad \beta_2 = h_2 \lambda a_2^*$$

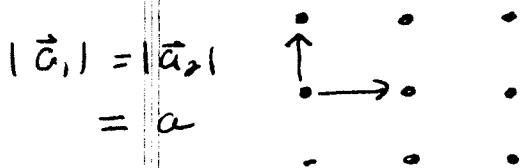
can do with single  $\lambda$



(0,0) independent of  $\lambda$   
 so easy to measure if not  $\perp$ .

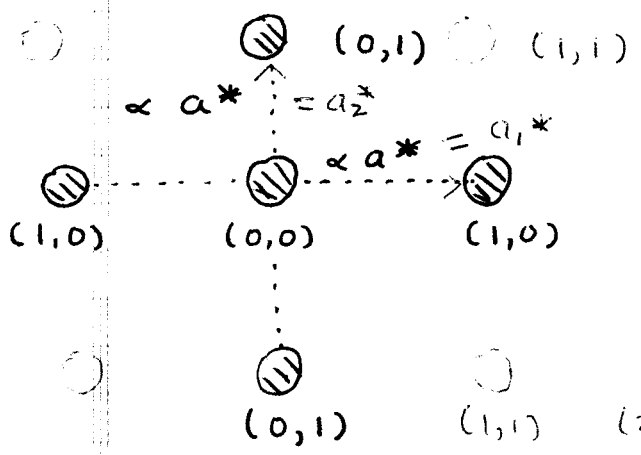
SIMPLE EXAMPLES

(a) Primitive cubic: no reconstruction of 100 ( $\lambda \equiv 1$ )



1<sup>st</sup> order LEED pattern:  $a_1^* = \frac{1}{a_1} = \frac{1}{a} = a^*$

$$a_2^* = \frac{1}{a_2} = \frac{1}{a} = a^*$$



⊙ Add higher orders  
"inverse net"

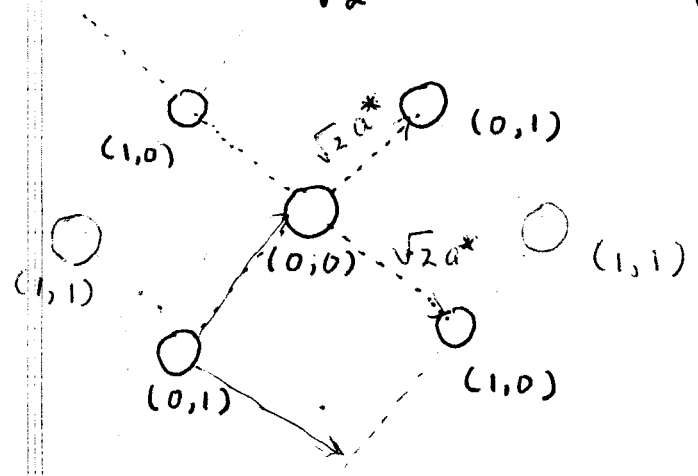
Increase  $\lambda \Rightarrow$  Increase Size of spacing

(b) fcc (100)

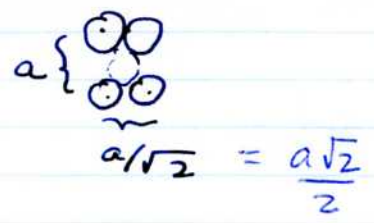
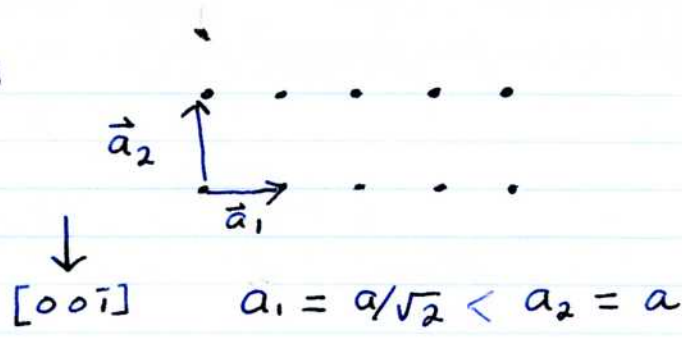


$$a_1 = \frac{\sqrt{2}}{2} a \quad a_2 = \frac{\sqrt{2}}{2} a$$

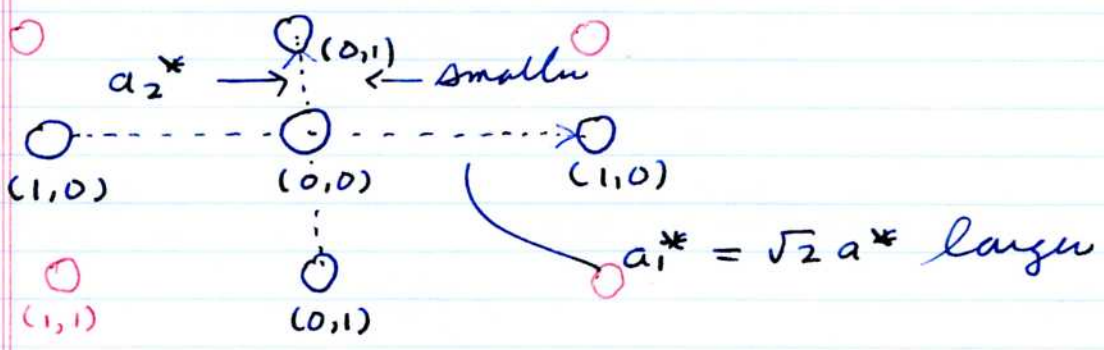
$$a_1^* = \frac{2}{\sqrt{2}} a^* \quad a_2^* = \frac{2}{\sqrt{2}} a^*$$



c) fcc (110)



REFLEXES:  $a_1^* = \sqrt{2} a^* > a_2^* = a^*$

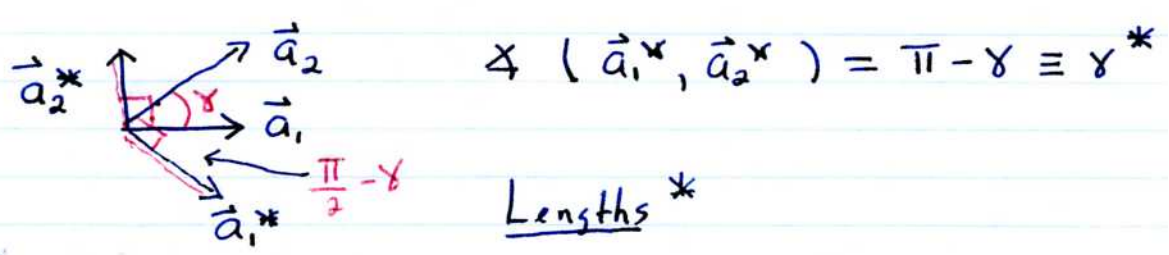


Non-Orthogonal Axes

A general relation to define the inverse mesh is:  $\vec{a}_i \cdot \vec{a}_j^* = \delta_{ij}$

$\vec{a}_1 \perp \vec{a}_2^*$   
 $\vec{a}_2 \perp \vec{a}_1^*$

preserve right-handedness



$$\vec{a}_1 = a_1 \vec{i} \quad \vec{a}_2 = a_2 (\cos \gamma \vec{i} + \sin \gamma \vec{j})$$

$$\vec{a}_1^* = a_1^* (\cos (\pi/2 - \gamma) \vec{i} - \sin (\pi/2 - \gamma) \vec{j})$$

$$\vec{a}_1 \cdot \vec{a}_1^* = \delta_{11} = 1 = a_1 a_1^* \cos (\pi/2 - \gamma) = a_1 a_1^* \sin \gamma$$

$$\therefore a_1^* = \frac{1}{a_1 \sin \gamma}$$

\* don't really need  $\vec{i}, \vec{j}$  analysis - see next page

Lengths w/o Vectors

$$\vec{a}_1 \cdot \vec{a}_1^* = 1 = a_1 a_1^* \cos(\pi/2 - \gamma) = a_1 a_1^* \sin \gamma$$

$$a_1^* = \frac{1}{a_1 \sin \gamma}$$

$$\vec{a}_2 \cdot \vec{a}_2^* = 1 = a_2 a_2^* \cos(\pi/2 - \gamma) = a_2 a_2^* \sin \gamma$$

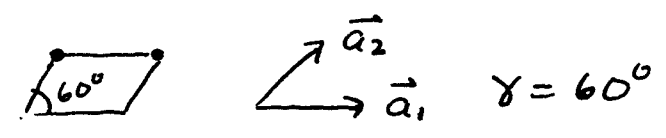
$$a_2^* = \frac{1}{a_2 \sin \gamma}$$

spreads out inverse net

Similarly  $\vec{a}_2 \cdot \vec{a}_2^* = 1 \Rightarrow a_2 a_2^* \sin \gamma = 1$

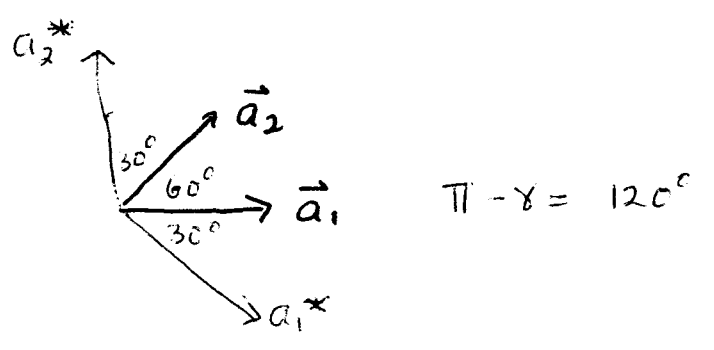
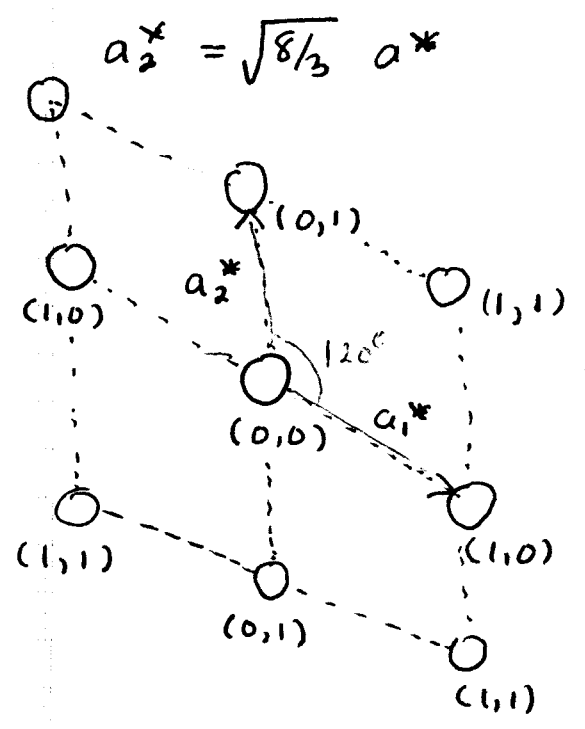
$a_2^* = \frac{1}{a_2 \sin \gamma}$  spreads out inverse net

Example: fcc (111)



$a_1 = a/\sqrt{2}$     $a_2 = a/\sqrt{2}$     $\sin 60^\circ = \sqrt{3}/2$

$a_1^* = \frac{1}{a_1 \sin \gamma} = \frac{\sqrt{2}}{a \sqrt{3}/2} = \frac{2\sqrt{2}}{a\sqrt{3}} = \sqrt{\frac{8}{3}} a^*$



(look on opposite side of paper: inverse mesh not really different from normal mesh)

(inverse same)

Adsorbate / Substrate Problems (-Inverse)

$\vec{a}_1, \vec{a}_2$  substrate    $\vec{b}_1, \vec{b}_2$  adsorbate   can be done without matrices

$\vec{b}_1 = G_{11} \vec{a}_1 + G_{12} \vec{a}_2$

$\vec{b}_2 = G_{21} \vec{a}_1 + G_{22} \vec{a}_2$

$\begin{pmatrix} \vec{b}_1 \\ \vec{b}_2 \end{pmatrix} = \begin{pmatrix} G_{11} & G_{12} \\ G_{21} & G_{22} \end{pmatrix} \begin{pmatrix} \vec{a}_1 \\ \vec{a}_2 \end{pmatrix}$

matrix approach requires primitive lattice MUST BE COMMENSURATE

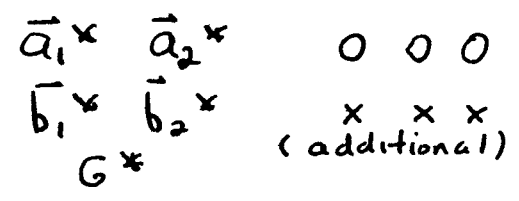
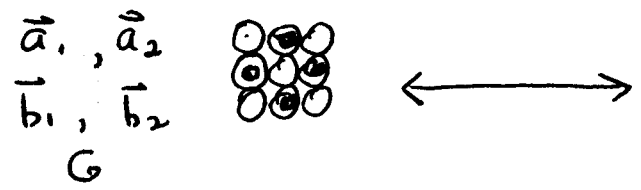
Also: 
$$\begin{pmatrix} \vec{b}_1^* \\ \vec{b}_2^* \end{pmatrix} = \begin{pmatrix} G_{11}^* & G_{12}^* \\ G_{21}^* & G_{22}^* \end{pmatrix} \begin{pmatrix} \vec{a}_1^* \\ \vec{a}_2^* \end{pmatrix}$$

$$G = ([G^*]^{-1})^\dagger = \frac{1}{|G^*|} \begin{pmatrix} G_{22}^* & -G_{21}^* \\ -G_{12}^* & G_{11}^* \end{pmatrix}$$

$$|G^*| = G_{11}^* G_{22}^* - G_{12}^* G_{21}^*$$

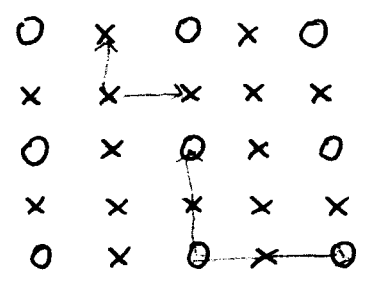
Real Space

Inverse Space (LEEDM)



Example: Inverse Problem

LEED Pattern  
 $\theta = 0.25$  of 0  
on Cu(100) fcc



no reconstruction

$$\vec{b}_1^* = \frac{1}{2} \vec{a}_1^* \quad \vec{b}_2^* = \frac{1}{2} \vec{a}_2^*$$

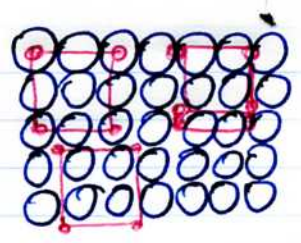
$$G^* = \begin{pmatrix} \frac{1}{2} & 0 \\ 0 & \frac{1}{2} \end{pmatrix} \quad |G^*| = \frac{1}{4}$$

$$G = \frac{1}{\frac{1}{4}} \begin{pmatrix} \frac{1}{2} & 0 \\ 0 & \frac{1}{2} \end{pmatrix} = \begin{pmatrix} 2 & 0 \\ 0 & 2 \end{pmatrix}$$

$$G \Rightarrow \vec{b}_1 = 2 \vec{a}_1 \quad \vec{b}_2 = 2 \vec{a}_2$$

While such a procedure allows an exact definition of the 2-D periodicity of the overlayer relative to the substrate, it says nothing about the actual adsorption sites:

$$\Theta = \frac{a_1 \times a_2}{b_1 \times b_2} ?$$



CN = 1, 2, or 4  
 $\text{Cu}(100) - \begin{bmatrix} 2 & 0 \\ 0 & 2 \end{bmatrix} - \text{O} - (0.25 \text{ ML})$

Note: to use matrix approach to determine LEED pattern;

$$G = ([G^*]^{-1})^t$$

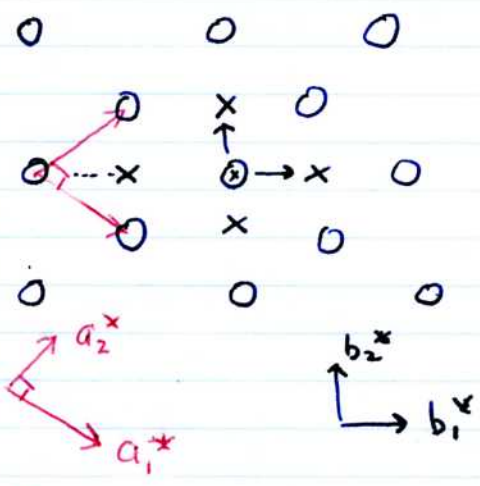
$$G^t = (G^*)^{-1}$$

$$(G^t)^{-1} = G^* = \begin{pmatrix} G_{11} & G_{21} \\ G_{12} & G_{22} \end{pmatrix}^{-1}$$

$$G^* = \frac{1}{|G|} \begin{pmatrix} G_{22} & -G_{21} \\ -G_{12} & G_{11} \end{pmatrix}$$

Example 2: slight variation 100 fcc again

LEED pattern



x - extra (adsorbate)

$$\vec{a}_1^* = \vec{b}_1^x - \vec{b}_2^x$$

$$\vec{a}_2^* = \vec{b}_1^x + \vec{b}_2^x$$

$$\vec{b}_1^x = \frac{1}{2} (\vec{a}_1^* + \vec{a}_2^*)$$

$$\vec{b}_2^x = \frac{1}{2} (-\vec{a}_1^* + \vec{a}_2^*)$$

$$a_1^* = \frac{2}{\sqrt{2}} a^*$$

$$a_2^* = \frac{2}{\sqrt{2}} a^*$$

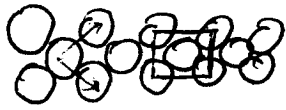
$$G^* = \begin{pmatrix} 1/2 & 1/2 \\ -1/2 & 1/2 \end{pmatrix}$$

$$G = \frac{1}{|G^*|} \begin{pmatrix} 1/2 & 1/2 \\ -1/2 & 1/2 \end{pmatrix} = \frac{1}{1/2} \begin{pmatrix} 1/2 & 1/2 \\ -1/2 & 1/2 \end{pmatrix}$$

$$G = \begin{pmatrix} 1 & 1 \\ -1 & 1 \end{pmatrix}$$

$$\vec{b}_1 = \vec{a}_1 + \vec{a}_2$$

$$\vec{b}_2 = -\vec{a}_1 + \vec{a}_2$$

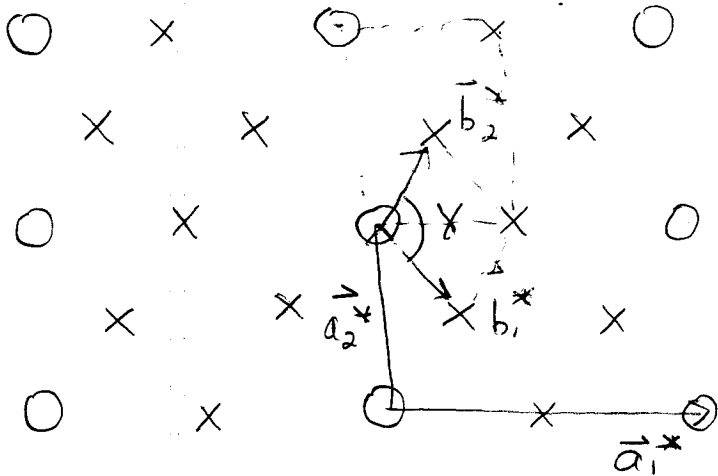


$$100 - \begin{bmatrix} 1 & 1 \\ -1 & 1 \end{bmatrix}$$

Ask  $\theta =$

### Inverse + Non-orthogonal

LEED

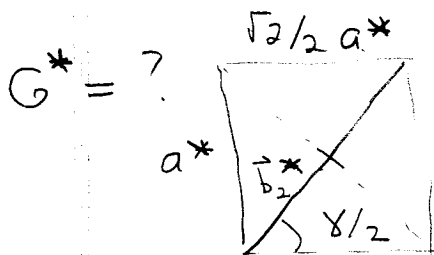


$$|\vec{a}_1^*| = \sqrt{2} |\vec{a}_2^*|$$

measured

$$|\vec{a}_1^*| = \sqrt{2} a^*$$

$$|\vec{a}_2^*| = a^*$$



$$\tan \gamma/2 = \frac{1}{\sqrt{2}/2}$$

$$\gamma/2 = \tan^{-1} \sqrt{2}$$

$$= 54.74^\circ$$

$$\gamma = 109.47^\circ$$

$$\vec{b}_1^* = +\frac{\sqrt{2}}{4} a^* \hat{i} - \frac{1}{2} a^* \hat{j}$$

$$\vec{b}_1^* = \frac{1}{4} \vec{a}_1^* - \frac{1}{2} \vec{a}_2^*$$

$$\vec{b}_2^* = \frac{1}{4} \vec{a}_1^* + \frac{1}{2} \vec{a}_2^*$$

$$G^* = \begin{pmatrix} 1/4 & -1/2 \\ 1/4 & 1/2 \end{pmatrix}$$

$$G = \frac{1}{|G^*|} \begin{pmatrix} 1/2 & -1/4 \\ 1/2 & 1/4 \end{pmatrix}$$

$$|G^*| = \frac{1}{8} - (-\frac{1}{8}) = \frac{1}{4}$$